

# Effect of Profiles and Shape on Ideal Stability of Advanced Tokamak Equilibria

*M. A. Makowski, T. A. Casper, J. R. Ferron, T. S. Taylor,  
A. D. Turnbull*

This article was submitted to: *30<sup>th</sup> EPS Conference on Controlled Fusion and Plasma Physics, St. Petersburg, Russia*  
07/07/2003 – 07/11/2003

U.S. Department of Energy

Lawrence  
Livermore  
National  
Laboratory

**July 7, 2003**

This document was prepared as an account of work sponsored by an agency of the United States Government. Neither the United States Government nor the University of California nor any of their employees, makes any warranty, express or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. Reference herein to any specific commercial product, process, or service by trade name, trademark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the United States Government or the University of California. The views and opinions of authors expressed herein do not necessarily state or reflect those of the United States Government or the University of California, and shall not be used for advertising or product endorsement purposes.

This work was performed under the auspices of the U.S. Department of Energy by University of California, Lawrence Livermore National Laboratory under Contract W-7405-Eng-48.

# Effect of Profiles and Shape on Ideal Stability of Advanced Tokamak Equilibria

M.A. Makowski<sup>1</sup>, T.A. Casper<sup>1</sup>, J.R. Ferron<sup>2</sup>, T.S. Taylor<sup>2</sup>, and A.D. Turnbull<sup>2</sup>

<sup>1</sup>*Lawrence Livermore National Laboratory, Livermore, California, 94550 USA*

<sup>2</sup>*General Atomics, P.O. Box 85608, San Diego, California 92186-5608 USA*

**Abstract.** The pressure profile and plasma shape, parameterized by elongation ( $\kappa$ ), triangularity ( $\delta$ ), and squareness ( $s$ ), strongly influence stability. In this study, ideal stability of single null and symmetric, double-null, advanced tokamak (AT) configurations is examined. All the various shapes are bounded by a common envelope and can be realized in the DIII-D tokamak. The calculated AT equilibria are characterized by  $P_0/P \sim 2.0$ –4.5, weak negative central shear, high  $q_{\min}$  ( $>2.0$ ), high bootstrap fraction, an H-mode pedestal, and varying shape parameters. The pressure profile is modeled by various polynomials together with a hyperbolic tangent pedestal, consistent with experimental observations. Stability is calculated with the DCON code and the resulting stability boundary is corroborated by GATO runs.

## 1. Introduction

Plasma boundary shape and the pressure profile are both known to strongly influence global stability. These parameters are especially important in advanced tokamak (AT) configurations. The effect of boundary shape and pressure profile is systematically studied with the aim of obtaining the optimal  $N$ .

We start with a specified pressure profile composed of a polynomial for the core plus a hyperbolic tangent function for the pedestal. The pressure peaking factor,  $P_0/P$ , is varied by varying  $b_n$  in the polynomial,  $P'_n(\psi) = -P'_{0n} [1 + b_n \psi - (1 + b_n) \psi^2]$  where  $\psi$  is the normalized poloidal flux,  $P'_n$  is the derivative of the pressure profile, and  $-P'_{0n}$  is its value at  $\psi = 0$ . The additive hyperbolic tangent function uses a pedestal pressure derived from a scaling law based on an experimental fit to DIII-D data. Model temperature and density profiles are then derived consistent with the pressure profile. The bootstrap current is computed using the NCLASS formulation together with the temperature and density profiles. A seed current that fills in the current profile at the center is added to the bootstrap current to fully specify the current profile. The seed current also has the effect of fixing  $q_0$  and is such as to produce weak negative central shear in the resulting  $q$ -profile.

Before the equilibrium can be obtained the boundary must be specified. A boundary of the form  $R = R_0 + a \cos[\theta + \sin^{-1} \delta \sin \theta]$ ,  $z = a \sin[\theta + \kappa_{o,i} \sin(2\theta)]$ , where  $R_0$  is the major radius,  $a$  is the minor radius,  $\delta$  the triangularity,  $\kappa$  the elongation, and  $\kappa_{o,i}$  are the outer and inner squareness. Having the pressure and current profiles specified together with the boundary, it is possible to solve for the equilibrium using the TEQ package in CORSICA. The resulting equilibria possess the following general characteristics of AT discharges: weak negative central shear with high  $q_{\min}$  ( $q_0 \sim 2.5$ –2.7 and  $q_{\min} \sim 2.1$ –2.4),  $f_{BS} \sim 0.70$ –0.95,  $I_p \sim 0.9$ –1.1 MA, and an H-mode edge pedestal.

Once the equilibrium has been computed, stability analysis is performed.  $n = 1$  and 2 ideal stability is calculated within CORSICA using the DCON package. Ballooning stability is evaluated using a ballooning package also contained within CORSICA. The GATO ideal stability code is also used to crosscheck  $n = 1, 2$  stability. For all stability calculations, an ideal conducting wall at the location of the DIII-D vacuum vessel is assumed. The various stability limits are found by incrementing the central pressure and repeating the above procedure. The entire process is repeated for each polynomial and value of shape parameter ( $\epsilon$ ,  $\delta$ , and  $\rho_0$ ). The parameter space encompassed by this study is  $\epsilon = 1.8, 1.9, 2.0$ ;  $\delta = 0.5, 0.65, 0.8$ ;  $\rho_0 = 0.0, 0.1, 0.2$ , and six polynomials ( $b_n = -2, -5/3, -4/3, -1, -1/2, 1$ ; the profile broadens with increasing  $b_n$ ) yielding a range of peaking factors of 2.0–4.5.

## 2. Stability Limits for Symmetric AT Equilibria

Figure 1(a,b) shows the global stability results. Figure 1(a) plots the  $n = 1$  beta limit as a function of the pressure peaking factor,  $P_0/P$  for the entire data set. In this case the maximum  $\beta_N$  clearly increases inversely with the peaking factor. A power law fit to the data is also shown in the plot and yields a relatively strong dependence on the peaking factor of  $(P_0/P)^{-1.32}$ . Similarly, Fig. 1(b) plots the  $n = 2$  beta limit. Here, the envelope of maximum  $\beta_N$  values also scales inversely with the peaking factor. However, due to the large variation with shape parameters, an exponent could not be inferred. At large peaking factors the limiting  $\beta_N$  tends to result from the  $n = 1$  mode, while at low peaking factors, it results from the  $n = 2$ . The crossover between the  $n = 1$  and 2 occurs at a peaking factor  $\sim 2.5$ .

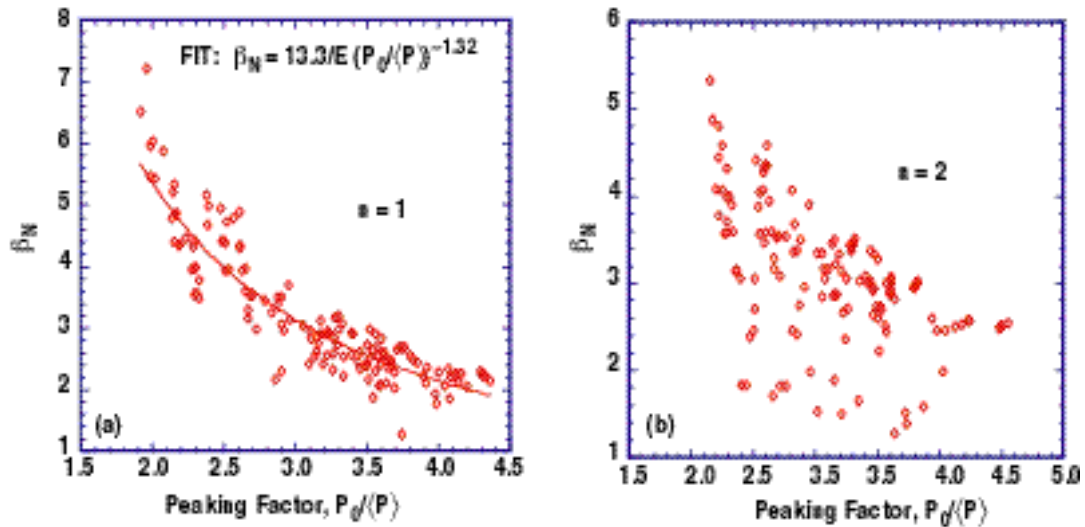


Fig. 1. Limiting  $\beta_N$  values for the  $n = 1$  (a) and  $n = 2$  (b) ideal modes as a function of  $P_0/P$  for all combinations of  $\epsilon$ ,  $\delta$ ,  $\rho_0$ , and peaking factor.

The lower values of  $\beta_N$  for the  $n = 2$  mode (in the range 1.5–2.5) generally correspond to a first-stability limit for equilibria with shape parameters at the extremes of their ranges, such as  $\epsilon = 0.8$  with  $\rho_0 = 0.0$ . As the pressure is increased, the  $n = 2$  mode generally stabilizes and a second  $n = 2$  limit is encountered in the  $\beta_N$  range of 3–5. In Fig. 1(b) only the lower of these two values of the  $n = 2$  -limit is plotted. The variation in the

data is higher than for the  $n = 1$  mode and increases with decreasing peaking factor. This remains true even if the lower  $\beta_N$  values are ignored. In general, the  $n = 1$  limit is dominated by profile effects, whereas shape plays a more significant role with respect to the  $n = 2$  limit, with the highest  $\beta_N$  values at a given peaking factor occurring for an optimal shape

Two ballooning unstable regions were often found to exist. The lower ballooning beta limit was found to be uniformly in the range 2.7–3.0 except at the lowest peaking factor where it increased abruptly to 5.5 for a restricted set of shapes.

As is evident in Fig. 1 there is a large variation in the data at any particular value of the peaking factor. This results from the complicated dependence of the beta limit on the shape factors,  $\delta$ ,  $\zeta_0$ , and  $\kappa$ , as well as on the details of the pressure profile through  $b_n$  as shown in Fig. 2. Here the  $n = 1$  and 2 limits are plotted versus  $\delta$  (at fixed  $\zeta_0$ ,  $\kappa$ , and peaking factor) and versus  $\zeta_0$  (at fixed  $\delta$ ,  $\kappa$ , and peaking factor). For the  $\delta$ -scan of Fig. 2(a), the maximum  $\beta_N$  is limited everywhere by the  $n = 1$  mode. In contrast, for the  $\zeta_0$ -scan of Fig. 2(b), the  $\beta_N$ -limit is set everywhere by the  $n = 2$  mode. The  $n = 1$   $\delta$ -scan shows an optimal intermediate value of  $\delta \sim 0.6$ , whereas the  $n = 2$   $\zeta_0$ -scan is monotone decreasing with  $\zeta_0$ . For the  $\delta$ -scan, an  $n = 1$  internal mode actually sets the  $\beta_N$ -limit at  $\delta = 0.8$ .

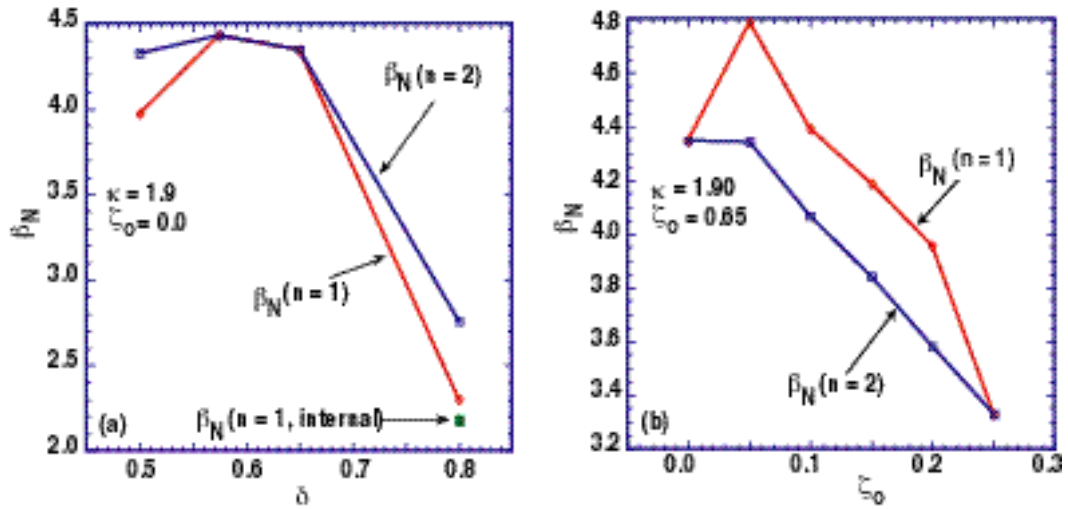


Fig. 2. Parameter scans of maximum  $\beta_N$  vs  $\delta$  at fixed  $\zeta_0$  and  $\kappa$  (a) and vs  $\zeta_0$  at fixed  $\delta$  and  $\kappa$ . The peaking factor is  $\sim 2.5$  for both (a) and (b).

Figure 3 shows a parameter scan of  $\beta_N$ -limit for the  $n = 1$  and 2 modes versus  $\delta$  for several values of  $\zeta_0$  at fixed  $\kappa$  and peaking factor. The  $n = 2$  mode always sets the  $\beta_N$ -limit. Again the parametric dependence is complicated. Increasing  $\zeta_0$  leads to a higher  $\beta_N$ -limit except at the largest squareness. Considering all cases the  $\beta_N$ -limit is 4.6 for a peaking factor of  $\sim 2.5$  with  $\delta = 2.0$ ,  $\zeta_0 = 0.65$ , and  $\kappa = 0$ , and results from an  $n = 2$  mode.

The ideal stability code GATO was used to check some of the DCON results presented here. For the six cases studied, corresponding to the  $\zeta_0$  parameter scan of Fig. 2(b), the  $\beta_N$ -limits either agree exactly or differ by at most 10%, with DCON generally predicting a slightly higher  $\beta_N$ -limit than GATO.

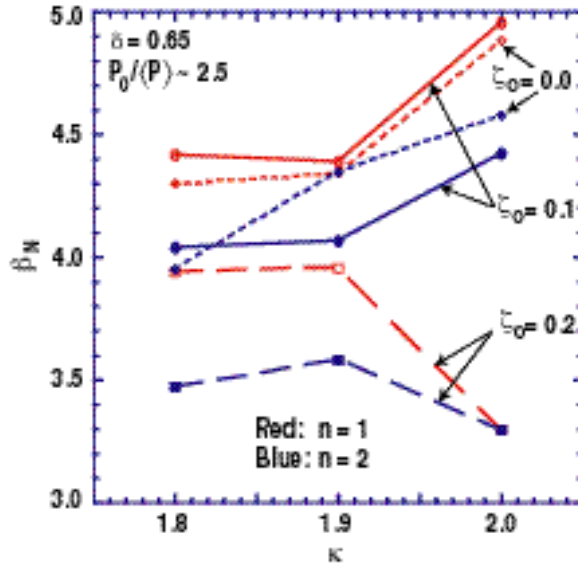


Fig. 3. Parameter scan of maximum  $\beta_N$  vs  $\kappa$  at fixed  $\beta_0/(P) \sim 2.5$  and peaking parameter

### 3. Stability Limits of Asymmetric Equilibria

In addition to the above previously discussed equilibria, the ideal stability of some up/down asymmetric equilibria was also examined. Two such shapes are shown in Fig. 4. These shapes are chosen to couple to the

upper (106975) and lower (163111) divertors in DIII-D. (The latter is only a proposed shape at this time, whereas the former has been used in experiments). Stability analysis of these equilibria yields the following  $\beta_N$ -limits corresponding to a peaking factor of  $\sim 2.5$ . For 106975 the  $\beta_N$ -limits are 2.67, 2.98, and 2.98 respectively for the  $n = 1, 2$ , and ballooning modes (limiting value is  $\beta_N = 2.67$ ). Similarly, for 163111 the  $\beta_N$ -limits are 3.85, 3.85, and 4.59 respectively (limiting  $\beta_N = 3.85$ ). Both limiting  $\beta_N$ s for these specific shapes are  $\sim 25\%$  below the optimum found above for the symmetric equilibria

### 4. Conclusions

Plasma boundary shape and the pressure profile are important for determining global plasma stability. The pressure profile plays a significant role in setting the  $\beta_N$ -limits for the  $n = 1$  and 2 modes, particularly the former. Shape plays a greater role in setting the  $n = 2$  stability limit. The optimum  $\beta_N$  is a complex function of the shape parameters  $\epsilon_0$ ,  $\kappa$ , and  $\beta_0/(P)$ . GATO and DCON agree quite well on both the  $n = 1$  and 2 stability limits. This fact has made this study possible as stability analysis of all the cases with GATO alone would have been prohibitive in terms of time

Work supported by U.S. Department of Energy under Contract DE-AC03-99ER54463, and Grants DE-FG03-97ER54415, DE-FG02-92ER54141, DE-FG03-96ER54373, and DE-FG03-01ER54615.

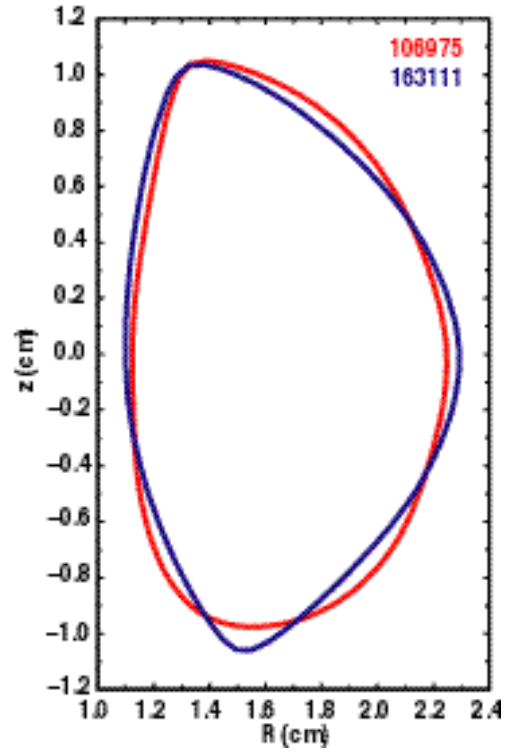


Fig. 4. Asymmetric equilibria optimized to couple of the upper (106975) and lower (163111) divertors in DIII-D.